

LA-UR-17-27526 (Accepted Manuscript)

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Provided by the author(s) and the Los Alamos National Laboratory (2017-12-08).

**To be published in:** Nuclear Instruments and Methods in Physics Research Section A: Accelerators, Spectrometers, Detectors and Associated Equipment

**DOI to publisher's version:** 10.1016/j.nima.2017.09.025

**Permalink to record:** <http://permalink.lanl.gov/object/view?what=info:lanl-repo/lareport/LA-UR-17-27526>

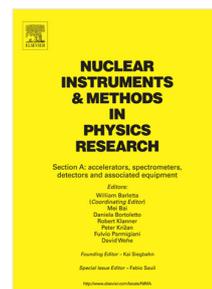
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PII: S0168-9002(17)30995-6  
DOI: <http://dx.doi.org/10.1016/j.nima.2017.09.025>  
Reference: NIMA 60104

To appear in: *Nuclear Inst. and Methods in Physics Research, A*

Received date: 25 August 2017  
Accepted date: 13 September 2017

Please cite this article as: M. Lockhart, D. Henzlova, S. Croft, T. Cutler, A. Favalli, C. McGahee, R. Parker, Experimental evaluation of the extended Dytlewski-style dead time correction formalism for neutron multiplicity counting, *Nuclear Inst. and Methods in Physics Research, A* (2017), <http://dx.doi.org/10.1016/j.nima.2017.09.025>

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1 Experimental Evaluation of the Extended Dytlewski-Style Dead Time Correction  
2 Formalism for Neutron Multiplicity Counting

3

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5

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10

11 Abstract

12 Over the past few decades, neutron multiplicity counting has played an integral role in Special  
13 Nuclear Material (SNM) characterization pertaining to nuclear safeguards. Current neutron  
14 multiplicity analysis techniques use singles, doubles, and triples count rates because a  
15 methodology to extract and dead time correct higher order count rates (i.e. quads and pents) was  
16 not fully developed. This limitation is overcome by the recent extension of a popular dead time  
17 correction method developed by Dytlewski. This extended dead time correction algorithm,  
18 named Dytlewski-Croft-Favalli (DCF), is detailed in reference [1], which gives an extensive  
19 explanation of the theory and implications of this new development. Dead time corrected results  
20 can then be used to assay SNM by inverting a set of extended point model equations which as  
21 well have only recently been formulated. The current paper discusses and presents the  
22 experimental evaluation of practical feasibility of the DCF dead time correction algorithm to  
23 demonstrate its performance and applicability in nuclear safeguards applications. In order to test  
24 the validity and effectiveness of the dead time correction for quads and pents, <sup>252</sup>Cf and SNM

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25 sources were measured in high efficiency neutron multiplicity counters at the Los Alamos  
26 National Laboratory (LANL) and the count rates were extracted up to the fifth order and  
27 corrected for dead time. In order to assess the DCF dead time correction, the corrected data is  
28 compared to traditional dead time correction treatment within INCC. The DCF dead time  
29 correction is found to provide adequate dead time treatment for broad range of count rates  
30 available in practical applications.

31

32 Keywords: neutron multiplicity counting, dead time correction, quads, pents

33

#### 34 1. Introduction

35 The identification and characterization of Special Nuclear Materials (SNM) is essential in  
36 safeguards measurements performed by the Department of Energy (DOE) and other agencies.  
37 SNM such as plutonium and uranium have unique signatures based on the emission of correlated  
38 neutrons from spontaneous or induced fission and many Non-Destructive Assay (NDA)  
39 techniques can be used to detect and extract the correlated rates to detect, identify, and quantify  
40 SNM. Current methods of correlated neutron counting are based on measurement of singles ( $S$ ),  
41 correlated pairs (doubles,  $D$ ) and, in multiplicity counting, correlated triplets (triples,  $T$ ) [2].  
42 Using the extracted correlated count rates, SNM can be characterized using point model  
43 equations, which relate the neutron coincidences to the properties of an item and allow for the  
44 calculation of  $^{240}\text{Pu}$  effective mass, leakage multiplication, and random neutron contribution  
45 from  $(\alpha, n)$  interactions in the item [2,3].

46 Passive Neutron Multiplicity Counting (PNMC) based on correlated rates up to triples is a highly  
47 developed and widely used assay method to quantify SNM forming a pillar of technical nuclear  
48 safeguards. However, with improved data acquisition techniques and analysis methods, the  
49 practical feasibility and implications of extending the neutron multiplicity counting beyond  
50 triples can now be assessed. Addition of higher order correlated rates (quads and pents) can  
51 expand experimental information that can in turn be used in the improved characterization of  
52 SNM. With high efficiency neutron multiplicity counters there is potential to measure higher  
53 order correlated rates, quads and pents, if current methods of analysis are extended to include  
54 their explicit calculation for utilization in SNM characterization. To be able to use these  
55 additional observables in practical applications, dedicated dead time correction algorithms must  
56 be developed. Both of these aspects were addressed in recently developed advanced dead time  
57 correction algorithm based on the popular dead time correction method developed by Dytlewski  
58 [4]. The Dytlewski-Croft-Favalli (DCF) dead time correction algorithm [1] was developed at Los  
59 Alamos National Laboratory (LANL) and extends the PNMC towards higher order correlated  
60 rates with self-consistent treatment of dead time. To actually use the dead time corrected quads  
61 and pents to assay SNM properties, extended point model equations have also recently been  
62 developed [5]. Evaluation of these equations and quads and pents importance in SNM  
63 characterization represents a separate subject of research and will be presented in a future  
64 publication.

65 The following sections present experimental evaluation of the DCF algorithm with the focus on  
66 1/ examination of the feasibility of quads and pents measurement and 2/ evaluation of  
67 performance of the DCF dead time correction. The second evaluation includes measurements of  
68  $^{252}\text{Cf}$  sources and plutonium items. While the  $^{252}\text{Cf}$  data is used to assess the DCF dead time

69 correction for full range of correlated rates (singles through pents), the plutonium measurements  
70 focus on DCF performance in the characterization of plutonium using standard point model  
71 equation (i.e. relying on singles through triples only).

72

## 73 2. DCF Dead Time Correction and Analysis Parameters

74 The Dytlewski formalism for dead time correction was originally developed to correct correlated  
75 neutrons up to triples [4]. The DCF dead time correction algorithm provides an extension of the  
76 original Dytlewski equations toward higher order correlated rates (quads and pents) and was  
77 described in full detail in [1]. In addition to extending the PNMC beyond triples counting, the  
78 DCF also includes self-consistent dead time treatment of singles through triples. The original  
79 Dytlewski scheme corrected singles in an ad hoc way using empirical expressions [6]. The DCF  
80 algorithm therefore provides room for improved performance over traditional approaches  
81 currently in use for dead time correction of singles through triples count rates; in particular it  
82 offers potential to correct for anomalous behaviors such as negative correlated count rates.  
83 Negative correlated count rates (triples and less often doubles) are experimentally observed in  
84 challenging measurement scenarios involving materials with very high neutron emission rates  
85 and cannot be appropriately corrected using existing empirical dead time correction methods.

86 The DCF remains simple to apply. It takes the form of matrix multiplication and is described by  
87 a single effective dead time parameter. Furthermore, the DCF algorithm was developed for all  
88 modes of neutron pulse train analysis and therefore extends the traditional PNMC beyond the  
89 standard shift register-based analysis. In the process of acquiring data from a multiplicity  
90 counter, one of two methods is used. The most common mode of data acquisition is through the

91 standard Multiplicity Shift Register (MSR). Another method is list mode data acquisition. The  
92 latter allows the complete neutron detection pulse train to be recorded and stored, making this  
93 approach the most flexible for data analysis [7]. With a complete record of all detection times,  
94 the data can be analyzed using a variety of approaches and is not limited by a reliance on MSR  
95 hardware. While MSR counting is limited to one method of analysis, data acquired in list mode  
96 can be analyzed with any of the following gating schemes: MIXED, RTI (Randomly-Triggered  
97 Inspection) and STI (Signal-Triggered Inspection).

98 The most widely used gating scheme in MSR counting is MIXED. This traditional analysis  
99 method combines information from signal-triggered gates and randomly-triggered gates to  
100 extract correlated rates. In the signal-triggered gates, the gate opens with each incoming neutron  
101 pulse after a short pre-delay, which serves as a pause to allow the detection efficiency to return to  
102 normal after the disruption caused by the incoming event. In the randomly-triggered gates, the  
103 gates open independently from the time in which a pulse or signal arrives. The RTI approach is  
104 solely based on the latter method and represents a variant on an approach developed in the field  
105 of reactor noise analysis [8]. On the other hand, STI only utilizes information contained in the  
106 signal-triggered gates. Extension of these approaches into PNMC was presented in [9,10].

107 For randomly-triggered gates, the sampling frequency is also taken into consideration. The main  
108 sampling techniques include consecutive sampling, fast accidental sampling (FAS), and  
109 sampling at neutron detection frequency (i.e. corresponding to the frequency of signal-triggered  
110 gate openings). In the consecutive sampling technique, gates are triggered one after another with  
111 no overlap. In the case of FAS, gates are overlapping and triggered at a fixed frequency.

112 With DCF all of these approaches can be used to extract and dead time correct correlated rates  
113 up to pents. This allows for comparison among these approaches for any potential improvements

114 in the overall performance. Note that the STI method does not lend itself to a practical  
115 implementation [1] and therefore will not be included in this evaluation. The current  
116 experimental evaluation will focus on FAS sampling technique due to its improved statistical  
117 uncertainty over the other sampling methods [11].

118

## 119 2.1 Gate Width and Gate Utilization Factors

120 It was described in [12] that an optimum gate width can be determined for different modes of  
121 neutron pulse train analysis described above. However, the implementation of a variable  
122 optimum gate width in analysis is likely unrealistic in practical applications. In all current  
123 practical safeguards applications a single gate width is typically used. Therefore, for current  
124 analysis purposes, the gate width was set to a fixed value for each detector used for  
125 measurements and is specified in the detector parameters in Table 1.

126 Because the gate width is finite, all correlations may not be detected within the gate time. Taking  
127 into account the die-away time ( $\tau$ ), pre delay ( $T_p$ ), and the gate width ( $T_g$ ) parameters of a given  
128 detector, the gate utilization factor (GUF), i.e. the fraction of correlated neutrons detected within  
129 the gate time period, can be calculated using Eq. 1 and 2. The MIXED GUF is defined for  
130 doubles through pents as  $f_n$ ,  $n=1-5$  (also denoted as  $n=d,t,q,\rho$  in some resources). Similarly, RTI  
131 GUF is denoted by  $w_n$ ,  $n=1-5$ . Note that  $f_1=w_1=1$ , meaning that the singles count rate is  
132 unaffected by the pre-delay and gate width. The determination of the GUF is vital because they  
133 are required in the RTI expressions for correlated rates that have been developed for the DCF  
134 correction [1] as well as in the point model expressions [2]. Note that DCF MIXED expressions  
135 for singles through pents are independent of GUF values; for the MIXED analysis GUF

136 knowledge is only required in the point model equations for extraction of the SNM  
 137 characteristics.

138

$$139 \quad f_n = [e^{-T_p/\tau}(1 - e^{-T_g/\tau})]^{n-1} = f_2^{n-1} \quad (\text{Eq. 1})$$

$$140 \quad w_n = \sum_{k=0}^{n-1} (-1)^k \binom{n-1}{k} \left( \frac{1 - e^{-kT_g/\tau}}{kT_g/\tau} \right) \quad (\text{Eq. 2})$$

141

142 Eq. 1 and 2 assume single die-away time approximation that is not always valid for neutron  
 143 multiplicity detectors and in practice [13], GUF values are therefore typically determined  
 144 experimentally [2]. However, it provides a good initial estimation and in the current analysis  
 145 theoretical GUF values will be used to maintain consistency among the different pulse train  
 146 analysis methods.

147

## 148 2.2 Dead Time Parameter and its Optimization

149 In order to use the DCF correction, an effective dead time parameter is required for each  
 150 detector. The value of this parameter may not necessarily be the same across the different pulse  
 151 train analysis methods. For the purpose of this analysis, the initial estimate for the dead time  
 152 parameter is based on the INCC multiplicity dead time parameter for each detector used in the  
 153 measurements. The values of these parameters are provided in Table 1.

154 To find the most suitable value of the dead time parameter for each analysis method and  
 155 detection system used in this paper, further optimization of the dead time parameter was

156 performed using a set of well characterized  $^{252}\text{Cf}$  sources. A set of  $^{252}\text{Cf}$  sources with varying  
157 neutron emission rates, but of similar age and impurities are a suitable choice because the  $^{252}\text{Cf}$   
158 sources do not have multiplication or random neutron contribution (i.e.  $(M=1)$  and  $(\alpha,n)=0$ ).  
159 Without multiplication and  $(\alpha,n)$  production, the point model equations are simplified  
160 significantly [2]. Under this presumption, the count rate ratios (i.e.  $D/S$ ,  $T/S$ ,  $Q/S$ ,  $P/S$ ) are  
161 theoretically proportional to powers of the detector efficiency and should therefore be constant  
162 with increasing source strength if the optimum dead time treatment is implemented. Such  
163 analysis is therefore strongly indicative of the quality of dead time correction treatment and also  
164 allows for optimization of the dead time parameter.

165

### 166 3. Experimental Evaluation

167

168 The key focus of this experimental evaluation is two-fold – 1/ to evaluate feasibility of higher  
169 order count rate measurements and 2/ to evaluate performance of the DCF dead time correction  
170 algorithm for practical applications. To evaluate both of these aspects, measurements were  
171 performed at LANL with three neutron multiplicity counters and a wide range of  $^{252}\text{Cf}$  and  $\text{PuO}_2$   
172 items. It is important that the counters have high neutron detection efficiency to extract higher  
173 order moments with less uncertainty and to allow investigation of feasibility of quads and pents  
174 measurements for practical applications.

175

176 The three detectors used were Epithermal Neutron Multiplicity Counter (ENMC) [14], ENMC  
177 with Inventory Sampling Counter (INVS) insert [15], and Advanced Recovery and Integrated  
178 Extraction System (ARIES) neutron counter [16]. ENMC and ENMC/INVS were used to

179 measure  $^{252}\text{Cf}$  sources while ARIES was used to measure  $\text{PuO}_2$  sources at an operating nuclear  
180 facility. The individual detector parameters are summarized in Table 1. The dead time  
181 coefficients (A, B,  $\delta$ ) were used in the standard INCC dead time correction [6] that serves as a  
182 reference for DCF performance.

183

184 {space for Table 1}

185

186 ENMC is a  $^3\text{He}$ -based detector containing 121  $^3\text{He}$  tubes arranged in 4 rings. The  $^3\text{He}$  tubes are  
187 1" (2.54 cm) in diameter and have an internal pressure of 10 atm. The central cavity is  
188 approximately 17.0" (43.2 cm) tall and 7.6" (19.4 cm) in diameter and the active length of the  
189 counter is 28.0" (71.1 cm). ENMC groups the 121 tubes into 27 channels equipped with  
190 AMPTEK amplifiers and a derandomizing buffer [17].

191 The performance of the ENMC is augmented by the addition of an INVS insert. The INVS was  
192 designed to be inserted into the sample chamber of ENMC for the assay of smaller items. It  
193 contains an additional 21  $^3\text{He}$  tubes arranged in two rings around the central cavity. The small  
194 sample chamber is 2.0" (5.1 cm) in diameter and 6.0" (15.2 cm) high and the active length of the  
195 insert is 20.0" (50.8 cm). With the insertion of the INVS, the efficiency of ENMC is increased by  
196 more than 20% relative, however it is limited to smaller diameter samples.

197 The ENMC and ENMC/INVS were used to measure series of  $^{252}\text{Cf}$  sources and each source was  
198 measured for 900 s. An overview of sources available for measurements is provided in Table 2.

199 The data from the ENMC and EMC/INVS counters was acquired in list mode using a Pulse  
200 Train Recorder (PTR32) list mode module that allows recording of up to 32 channels

201 simultaneously [7]. The key advantage of list mode acquisition is flexibility in data analysis of  
202 the recorded complete pulse train and was chosen to enable both, MIXED and RTI analysis  
203 methods to fully test the DCF algorithm capabilities.

204

205 {space for Table 2}

206

207 To demonstrate practical feasibility of the DCF dead time correction algorithm, it is also  
208 desirable to evaluate its performance on materials of operational interest. For this purpose a  
209 range of PuO<sub>2</sub> items with different masses was measured in the ARIES multiplicity counter that  
210 resides in an operating facility at LANL. An overview of the measured PuO<sub>2</sub> items is  
211 summarized in Table 3. The measurements corresponded to 1 hour and data were acquired using  
212 standard MSR electronics and INCC software. Only MIXED DCF analysis was performed on  
213 this dataset to provide a direct comparison with the empirical dead time correction within INCC.  
214 The detector parameters (pre-delay, gate and efficiency) used in the analysis were taken over  
215 from INCC in order to allow for a direct comparison and are listed in Table 1. The GUF values  
216 used in the point model equations to calculate <sup>240</sup>Pu effective mass were also taken from INCC  
217 and correspond to  $f_g=0.6640$ ,  $f_r=0.4482$ .

218

219 {space for Table 3}

220

221 3.1 Feasibility of Quads and Pents Measurements

222 In order to assess feasibility of quads and pents measurements, a range of  $^{252}\text{Cf}$  sources with  
223 increasing neutron emission rates was measured and corresponding quads and pents uncertainties  
224 were evaluated for a fixed measurement time corresponding to 900 s. Longer measurement time  
225 would decrease the uncertainty, but 900 s was selected as a representative of a typical NDA  
226 assay. The measurements were acquired as a series of 90 cycles of 10 s each to allow for sample  
227 based error estimation. The results for MIXED and RTI analysis for ENMC and ENMC/INVS  
228 are shown in Tables 4 and 5, respectively, to provide a direct comparison between the two  
229 analysis approaches. Both analyses were performed using FAS. The rates presented in this  
230 section are not corrected for dead time to provide an overview of measurement uncertainties for  
231 raw data. Implementation and effects of the DCF dead time correction for these higher order  
232 correlated rates will be discussed in the following section.

233

234 {space for Table 4 and 5}

235

236 The dead time uncorrected rates presented in Tables 4 and 5 also provide an important  
237 experimental demonstration of the effects of dead time on the measured higher order correlated  
238 rates. As can be seen in the ENMC dataset, quads and pents exhibit saturation trends or even turn  
239 to negative values with increasing count rate; an effect that was theoretically predicted in [18].  
240 The results presented in Tables 4 and 5 illustrate the complexity and challenges associated with  
241 reliable measurements of quads and pents. As can be seen in Table 4 and 5, a very good  
242 uncertainty (of the order of 5% or less) can be achieved in 900 s for quads for low to medium  
243 count rates (up to  $\sim 200$  kHz) for ENMC and for high count rates (up to  $\sim 1$  MHz) for higher  
244 efficiency ENMC/INVS. Uncertainties of pents for the same measurement time are noticeably

245 higher for all the measured  $^{252}\text{Cf}$  sources. In addition, pents uncertainties exhibit complex trends  
246 and can be prohibitively large for cases where measured pents turn to negative values. Note that  
247 saturation tendencies (or count rates turning negative) are generally observed for lower singles  
248 count rates as the multiplicity order increases. This is also confirmed by the ENMC data, where  
249 pents turn negative, an effect not seen in quads (nor doubles and triples) for the same singles  
250 count rate range. It can also be seen that the uncertainties for quads deteriorate with increasing  
251 measured count rates. Comparison of RTI and MIXED approaches reveals tendency towards  
252 slightly better uncertainties in the case of the RTI analysis, an observation in agreement with  
253 previous findings documented in [12].

254 Overall, the current results provide an initial assessment of the feasibility of experimental  
255 extraction of quads and pents. The results also demonstrate that for sufficiently high efficiency  
256 counters (>60% in this study), uncertainties of 5% or less can be achieved in quads for  
257 measurement times of the order of 900 s. Note that these uncertainties would drop to <1% level  
258 for a 2 hr measurement time, which may still be practically feasible in some applications. Pents  
259 present a more challenging scenario due to their 5<sup>th</sup> order dependence on the neutron detection  
260 efficiency. Although pents suffer from noticeably worse uncertainty over the 900 s measurement  
261 period, the full feasibility assessment can only be made once the actual requirements on  
262 uncertainty and its propagation into the final physics quantities (e.g. through the extended point  
263 model equations) are taken into account; an area that will be subject of further research.

### 264 3.2 Performance of DCF Dead Time Correction

265 The following results demonstrate the performance of the DCF dead time correction on series of  
266  $^{252}\text{Cf}$  sources and practical feasibility of this algorithm on a set of  $\text{PuO}_2$  materials of operational  
267 interest. The results presented here contain a comparison between dead time uncorrected data,

268 the DCF corrected data for both MIXED and RTI gating schemes with FAS, and INCC empirical  
269 dead time correction. The INCC dead time correction has only been developed for MIXED  
270 analysis algorithm up to triples and therefore the corresponding dead time corrected data is  
271 included for MIXED analysis only [6].

272 The DCF dead time correction was performed using an optimum dead time parameter selected  
273 for each analysis algorithm and detector combination. As discussed previously, the count rate  
274 ratios ( $D/S$ ,  $T/S$ ,  $Q/S$ , and  $P/S$ ) for the measured set of  $^{252}\text{Cf}$  sources should be constant and  
275 independent of the source strength. To find an optimum dead time parameter, its value was  
276 varied until an optimum was found based on this method. The initial dead time estimate for  
277 ENMC and ENMC/INVS corresponded to 37 ns and 100 ns, respectively, and was varied  
278 between 20-40 ns and 60-110 ns, respectively, to optimize the final dead time correction. The  
279 optimum dead time parameters for each detector are summarized in Table 6. The DCF dead time  
280 corrected results using the optimum dead time parameters are plotted with the uncorrected data  
281 and traditional INCC corrected results in Figures 1 and 2 for ENMC and ENMC/INVS,  
282 respectively. The ENMC/INVS dataset includes sources with very high count rates which extend  
283 the evaluation of the performance of the DCF algorithm towards more extreme measurement  
284 scenarios.

285 For the ENMC dataset the DCF corrected results exhibit rather constant trends, independent of  
286 source strength, for all correlated orders and both analysis methods (MIXED as well as RTI).  
287 The effect of dead time treatment relative to dead time uncorrected results is clearly visible. In  
288 addition, the DCF corrected results also demonstrate capability of this algorithm to correct for  
289 negative count rates observed in dead time uncorrected pents (Figure 1, bottom). The ENMC  
290 DCF results analyzed using MIXED approach (Figure 1, left) show very good agreement with

291 INCC for  $D/S$  as well as  $T/S$  ratios confirming validity of the DCF algorithm for this count rate  
292 range.

293 The ENMC/INVS dataset exhibits more complex trends. Evaluation of this set of high rate  $^{252}\text{Cf}$   
294 sources in a very high efficiency neutron counter provides a unique opportunity to access the  
295 effectiveness of DCF for more extreme experimental scenarios. In case of ENMC/INVS the  
296 optimum dead time parameter was chosen mainly based on the  $D/S$  ratios. The  $D/S$  trend is  
297 independent of source strength for both MIXED and RTI approaches, however ratios begin to  
298 increase as a function of count rate for the higher order correlations. It can be clearly seen that  
299 for count rate ratios beyond doubles the DCF exhibits upward trend for both, MIXED and RTI  
300 analysis. This suggests that a lower dead time parameter would be more appropriate for  
301 correcting triples through pents than required by optimum doubles correction. This is an  
302 interesting observation suggesting a potential dependence of dead time correction parameter on  
303 multiplicity order and will be further explored with more extensive datasets. A comparison with  
304 INCC highlights a similar trend also in this traditional dead time correction, where  $T/S$  ratio  
305 exhibits an upward trend similar to DCF. The  $D/S$  and  $T/S$  DCF results analyzed using MIXED  
306 approach (Figure 2, left) show very good agreement with INCC.

307 Overall, the ENMC results, that represent more typical count rate range in practical applications,  
308 indicate capability of DCF algorithm to effectively correct for dead time effects for all correlated  
309 rates. In addition, capability to correct for negative count rates observed in dead time uncorrected  
310 pents was demonstrated. The ENMC/INVS results provide a rather extreme case of count rates  
311 less often encountered in practical applications, which, however, represents an important test  
312 scenario for the full capability of the DCF. The ENMC/INVS DCF results for  $D/S$  and  $T/S$   
313 exhibit similar trends as INCC, generally validating the DCF performance. However, observed

314 trends for correlated rates beyond doubles indicate potential dependence of dead time correction  
315 parameter on multiplicity order.

316

317 {space for Figure 1 and 2}

318

319 To further test the implementation of DCF correction algorithm the practical application of the  
320 DCF dead time corrected correlated rates for SNM characterization was evaluated using datasets  
321 from plutonium bearing materials. The purpose of this evaluation is to determine the capability  
322 to extract and correct correlated count rates up to triples which are then used to calculate the  
323 effective mass of  $^{240}\text{Pu}$ .

324 For this evaluation, the ARIES neutron counter was used to measure a range of Pu items with  
325 masses up to ~4.5 kg at an operational nuclear facility. Because an equivalent set of  $^{252}\text{Cf}$  sources  
326 was not available in the facility for this counter, the multiplicity dead time parameter (50.7 ns)  
327 utilized in standard INCC dead time correction was used in the DCF formalism and varied to  
328 investigate its influence on the  $^{240}\text{Pu}_{\text{eff}}$  mass. As discussed earlier, only MIXED analysis was  
329 performed on this dataset to provide a direct comparison with the standard INCC results.

330 Figure 3 shows a comparison of the mass ratio of measured versus declared (known)  $^{240}\text{Pu}$   
331 effective ( $^{240}\text{Pu}_{\text{eff}}$ ) mass with the measured mass extracted using DCF dead time correction for  
332 several values of dead time parameter as well as using INCC dead time correction. As can be  
333 seen from Figure 3, the DCF results for dead time parameter of ~40.7 ns demonstrate good  
334 agreement with INCC. The dataset covers broad range of Pu masses up to ~4.5 kg and the results  
335 shown therefore provide an initial validation of the DCF algorithm performance and demonstrate

336 its capability to provide results in close agreement with INCC, a nuclear safeguards standard. In  
337 other words, the DCF approach has passed the initial test, namely that it can be used in a way  
338 that preserves established performance norms if that is the goal.

339

340 {space for Figure 3}

341

#### 342 4. Discussion

343 A summary of the optimum dead time parameter values for DCF for both analysis approaches  
344 (MIXED, RTI), and counters is shown in Table 6. Table 6 also includes the initial dead time  
345 parameter estimate based on the INCC multiplicity dead time parameter.

346

347 {space for Table 6}

348

349 Table 6 highlights that optimum dead time parameter is not necessarily the same for both  
350 analysis approaches (MIXED and RTI). In general, the MIXED analysis requires a higher value  
351 of the dead time parameter than RTI. Note that the optimum dead time parameter values for the  
352 MIXED approach are in very close agreement with the standard INCC multiplicity dead time  
353 parameter. This further validates selection of the latter value for the DCF analysis of PuO<sub>2</sub>  
354 materials measured in the ARIES counter.

355 It should be pointed out that the DCF expressions for the RTI rates depend on the corresponding  
356 GUF values [1]. As described in section 2.1., theoretical GUF values were used in the current

357 evaluation. It can be anticipated that experimental GUF values could favor slightly different  
358 values of the RTI DCF dead time parameters, however it can be expected that the trends  
359 observed in the present evaluation (Figures 1-3) will remain largely unchanged. The choice of  
360 theoretical GUF values for this work was primarily motivated by a desire to maintain consistency  
361 among the different pulse train analysis methods and provides a robust initial assumption to  
362 assess the DCF performance for RTI analysis. A detailed study of experimental GUF values and  
363 their effect on the DCF RTI results will be subject of future work.

364 The optimum values of the dead time parameters presented in Table 6 were selected primarily  
365 based on the  $D/S$  ratio. However, the results in Figure 2 indicate a tendency towards lower  
366 optimum dead time parameter values for higher order correlated count rates, especially for quads  
367 and pents. This trend seems to be more pronounced for conditions more significantly affected by  
368 dead time, such as high count rates measured in high efficiency counters ENMC/INVS.

369 Although the optimum dead time parameter varies for fairly extreme count rates, the results  
370 shown in Figures 1-3 demonstrate that the DCF dead time corrected results provide adequate  
371 dead time treatment for typical measurement scenarios. In addition, the DCF extends the PNMC  
372 towards new capabilities in alternative analysis approaches (RTI) and extraction and dead time  
373 correction of higher order correlated rates.

374

## 375 5. Conclusions

376 This paper presented an experimental evaluation of performance of novel dead time correction  
377 algorithm based on traditional Dytlewski formalism. The DCF algorithm was developed to allow  
378 for extraction and dead time correction of higher order correlated rates (quads and pents) from

379 measured pulse train and also to provide improved performance over existing empirical dead  
380 time correction methods that cannot, for example, correct for anomalies such as negative count  
381 rates. The key motivation in extending traditional PNMC towards higher order correlated rates  
382 lies in the potential to improve characterization of assayed SNM via additional experimental  
383 observables. The capability to measure and use higher order moments represents a new area of  
384 research within nuclear safeguards and its full potential is still being explored. The current paper  
385 focused on key aspects of the DCF dead time correction algorithm in order to establish its  
386 performance for potential use in nuclear safeguards applications for all multiplicity orders from  
387 singles up to pents.

388 The paper explored two key areas – 1/ evaluation of feasibility to experimentally extract quads  
389 and pents with sufficient uncertainty and 2/ performance evaluation of DCF dead time correction  
390 algorithm for all count rates from singles up to pents.

391 To appropriately address the two key questions, high efficiency neutron multiplicity counters  
392 were used for the measurements. The evaluation of measured quads and pents was performed on  
393 dead time uncorrected data to remove any uncertainties associated with the correction and reveal  
394 magnitude of the dead time effects. The measured quads and pents and their corresponding  
395 uncertainties for 900 s measurement time demonstrated statistically meaningful results for quads  
396 with uncertainties of ~5% or less over a broad range of count rates (0.3 – 1,000 kHz). The  
397 observed uncertainties for pents were noticeably worse (greater than tens of percent). Both,  
398 quads and pents exhibited saturation and also negative values with increasing count rate, that  
399 clearly require sophisticated dead time correction treatment to fully recover. The high pents  
400 uncertainties and often negative values represent an important observation that may indicate

401 limited applicability of this experimental observable to certain measurement scenarios (high  
402 efficiency, however more moderate (< 100 kHz) neutron emission rates).

403 The evaluation of the DCF dead time correction included comparison of DCF dead time  
404 corrected count rate ratios ( $D/S$ ,  $T/S$ ,  $P/S$ , and  $Q/S$ ) with uncorrected and (where applicable)  
405 INCC dead time corrected results. The correction was studied on series of well-characterized  
406  $^{252}\text{Cf}$  sources as well as range of  $\text{PuO}_2$  items of operational mass range and included both,  
407 standard MSR analysis (MIXED) and alternative analysis based on randomly triggered gates  
408 only (RTI). The results revealed a very good performance of DCF over standard count rate range  
409 and for the broad range of  $\text{PuO}_2$  items with masses up to 4.5 kg. In particular, good agreement  
410 with INCC type dead time correction was observed for the measured  $^{252}\text{Cf}$  sources and  $\text{PuO}_2$   
411 materials. This serves as a demonstration of capability of DCF to correct for dead time effects in  
412 majority of measurement scenarios including items of practical interest. In addition, DCF  
413 demonstrated capability to correct negative count rates observed for some quads and pents.

414 High count rate measurement scenarios (500 – 1,000 kHz) were also evaluated with range of  
415  $^{252}\text{Cf}$  sources measured in 80% efficiency neutron counter. These results indicated potential  
416 dependence of dead time correction parameter on multiplicity order with lower dead time  
417 parameter values favored by higher order correlated rates (triples – pents) compared to doubles  
418 rates. A full implication and magnitude of this effect will have to be further evaluated.

419 The results presented provide a critical first step in the overall assessment of whether it is  
420 feasible to use quads and pents in practical safeguards measurements. They will be further  
421 explored in conjunction with advanced analysis models currently under development to fully  
422 assess the quads and pents measurement feasibility and their uncertainty limits for practical use.  
423 Further work will also focus on evaluation of influence of GUF values on the DCF RTI results.

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425

## 426 6. Acknowledgements

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428 This work was sponsored by the U.S. Department of Energy (DOE), National Nuclear Security  
429 Administration (NNSA), Office of Nonproliferation Research and Development (NA-22). We  
430 thank Dr. Peter Santi and Dr. Bill Geist for encouraging and supporting this work.

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497 List of Figures:

498 Figure 1: DCF corrected count rate ratios for a set of  $^{252}\text{Cf}$  sources measured in ENMC as a function of  
499 singles rate. INCC comparison is only available for MIXED results. Error bars for  $D/S$  and  $T/S$  are  
500 smaller than the size of the symbols.

501

502 Figure 2: DCF corrected count rate ratios for a set of  $^{252}\text{Cf}$  sources measured in ENMC/INVS as a  
503 function of singles rate. INCC comparison is only available for MIXED results. Note that dead time  
504 uncorrected  $Q/S$  and  $P/S$  ratios are shown on the right axis. Error bars for  $D/S$  and  $T/S$  are smaller than the  
505 size of the symbols.

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507 Figure 3: Measured versus declared  $^{240}\text{Pu}_{\text{eff}}$  mass extracted using DCF dead time correction algorithm  
508 compared with INCC.

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520 List of Tables:

Detector	Pre- delay [ s]	Gate Width [ s]	Die- away [ s]	Efficiency [%]	Dead Time Coefficient A (1E-6) [s]	Dead Time Coefficient B (1E-12) [s]	Multiplicity Dead Time $\delta$ [ns]
ENMC	1.5	24	21.8	65.0	0.0954	0.0289	36.8
ENMC/INVS	1.5	24	18.8	80.0	0.341	0.017	100.0
ARIES	3.0	64	51.0	51.8	0.182	0.000	50.7

521 Table 1: Operating parameters of multiplicity counters used in the evaluation.

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Table 2: Overview of neutron emission rates of measured  $^{252}\text{Cf}$  sources.

Source ID	Neutron emission rate [n/s]	Multiplicity counter	date
Cf4	6.7E+02	ENMC	01/01/2010
Cf11	6.8E+04	ENMC	01/01/2010
Cf12	1.3E+05	ENMC	01/01/2010
A7-866	2.6E+05	ENMC	01/01/2010
A7-867	5.1E+05	ENMC	01/01/2010
FTC-CF-1184	4.8E+05	ENMC/INVS	07/11/2016
FTC-CF-5065	1.1E+06	ENMC/INVS	07/11/2016
FTC-CF-2593	1.2E+06	ENMC/INVS	07/11/2016
FTC-CF-3097	2.0E+06	ENMC/INVS	07/11/2016

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553 Table 3: Overview of the known characteristics of the PuO<sub>2</sub> materials measured in the ARIES system.

Source ID	Declared	Declared <sup>240</sup> Pu
	Pu mass	effective mass
	[g]	[g]
Pu1	748.7	45.4
Pu2	1492.6	90.8
Pu3	2996.4	181.6
Pu4	4430.7	260.1

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571 Table 4: Singles count rate and correlated count rates for quads and pents for MIXED (top) and RTI

572 (bottom) analysis methods with corresponding uncertainties for  $^{252}\text{Cf}$  sources measured in ENMC.

Source	$S_{\text{MIXED}}$	$\sigma$ [%]	$Q_{\text{MIXED}}$	$\sigma$ [%]	$P_{\text{MIXED}}$	$\sigma$ [%]
Cf4	$426 \pm 1$	0.29	$20.7 \pm 0.4$	1.8	$2.7 \pm 0.2$	6.6
Cf11	$43,690 \pm 30$	0.07	$2,020 \pm 55$	3	$222 \pm 72$	32
Cf12	$83,739 \pm 18$	0.02	$3,467 \pm 110$	3	$13 \pm 182$	1,422
A7866	$167,104 \pm 24$	0.01	$5,227 \pm 302$	6	$-1,637 \pm 560$	34
A7867	$322,203 \pm 34$	0.01	$4,332 \pm 787$	18	$-6,420 \pm 1,983$	31
Source	SRTI	$\sigma$ [%]	QRTI	$\sigma$ [%]	PRTI	$\sigma$ [%]
Cf4	$426 \pm 1$	0.29	$24.1 \pm 0.8$	3.2	$3.8 \pm 0.8$	21.0
Cf11	$43,691 \pm 30$	0.07	$2,134 \pm 44$	2	$171 \pm 54$	32
Cf12	$83,739 \pm 18$	0.02	$3,624 \pm 93$	3	$-32 \pm 137$	427

A7866	167,102 ± 24	0.01	5,195 ± 247	5	-1,469 ± 442	30
A7867	322,203 ± 33	0.01	2,545 ± 649	26	-6,780 ± 1,503	22

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581 Table 5: Singles count rate and correlated count rates for quads and pents for MIXED (top) and RTI  
582 (bottom) analysis methods with corresponding uncertainties for <sup>252</sup>Cf sources measured in ENMC/INVS.

Source	S <sub>MIXED</sub>	σ [%]	Q <sub>MIXED</sub>	σ [%]	P <sub>MIXED</sub>	σ [%]
FTC-CF-1184	410,699 ± 42	0.010	-21,287 ± 1,280	6	-16,273 ± 3,433	21
FTC-CF-5065	910,678 ± 58	0.006	-80,018 ± 4,680	6	21,956 ± 13,732	63
FTC-CF-2593	985,405 ± 57	0.006	-85,939 ± 5,007	6	17,917 ± 15,042	84
FTC-CF-3097	1,566,867 ± 63	0.004	-75,923 ± 8,442	11	78,696 ± 32,485	41
Source	S <sub>RTI</sub>	σ [%]	Q <sub>RTI</sub>	σ [%]	P <sub>RTI</sub>	σ [%]
FTC-CF-1184	410,699 ± 42	0.010	-27,283 ± 899	3	-13,280 ± 2,065	16
FTC-CF-5065	910,679 ± 58	0.006	-75,972 ± 3,150	4	29,520 ± 8,042	27
FTC-CF-2593	985,406 ± 56	0.006	-74,242 ± 3,545	5	38,864 ± 9,167	24
FTC-CF-3097	1,566,867 ± 63	0.004	-13,231 ± 6,137	-46	84,224 ± 19,951	24

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Table 6: Summary of dead time parameters for each counter used in the evaluation of  $^{252}\text{Cf}$  data.

Detector	INCC Dead time estimate [ns]	DCF MIXED [ns]	DCF RTI [ns]
ENMC	37	40	30
ENMC/INVS	100	105	70

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Figure1

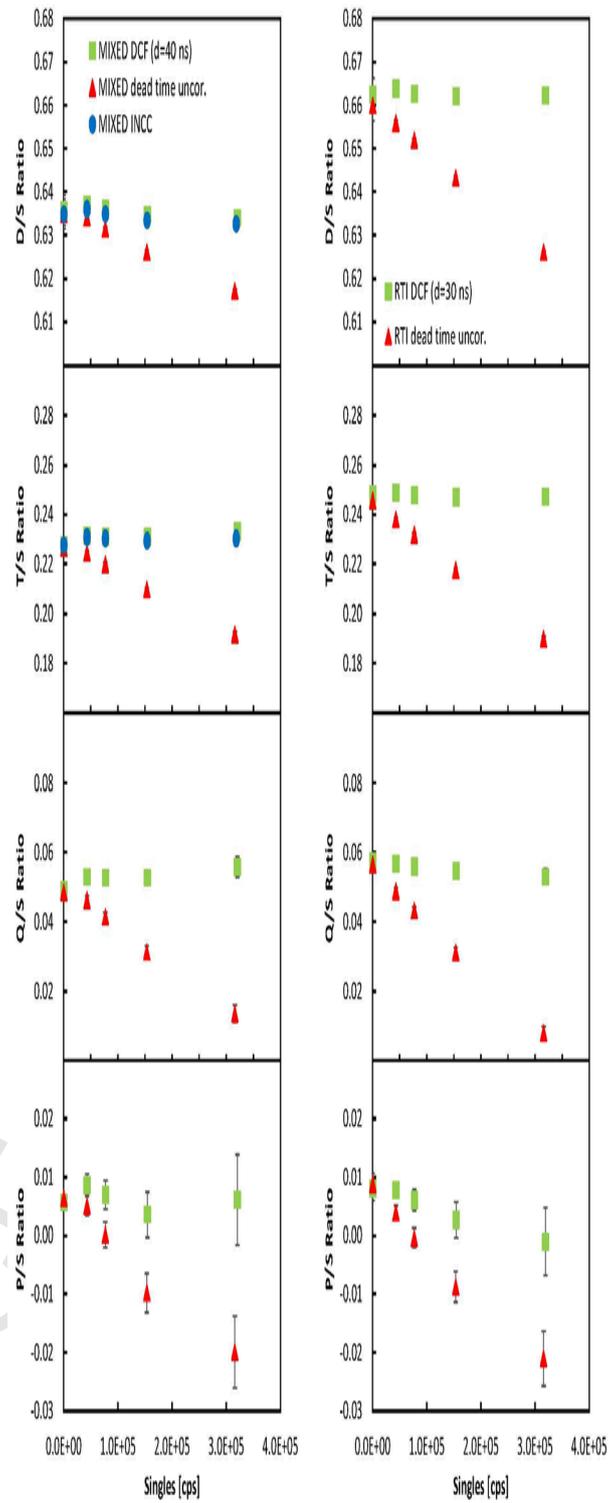


Figure2

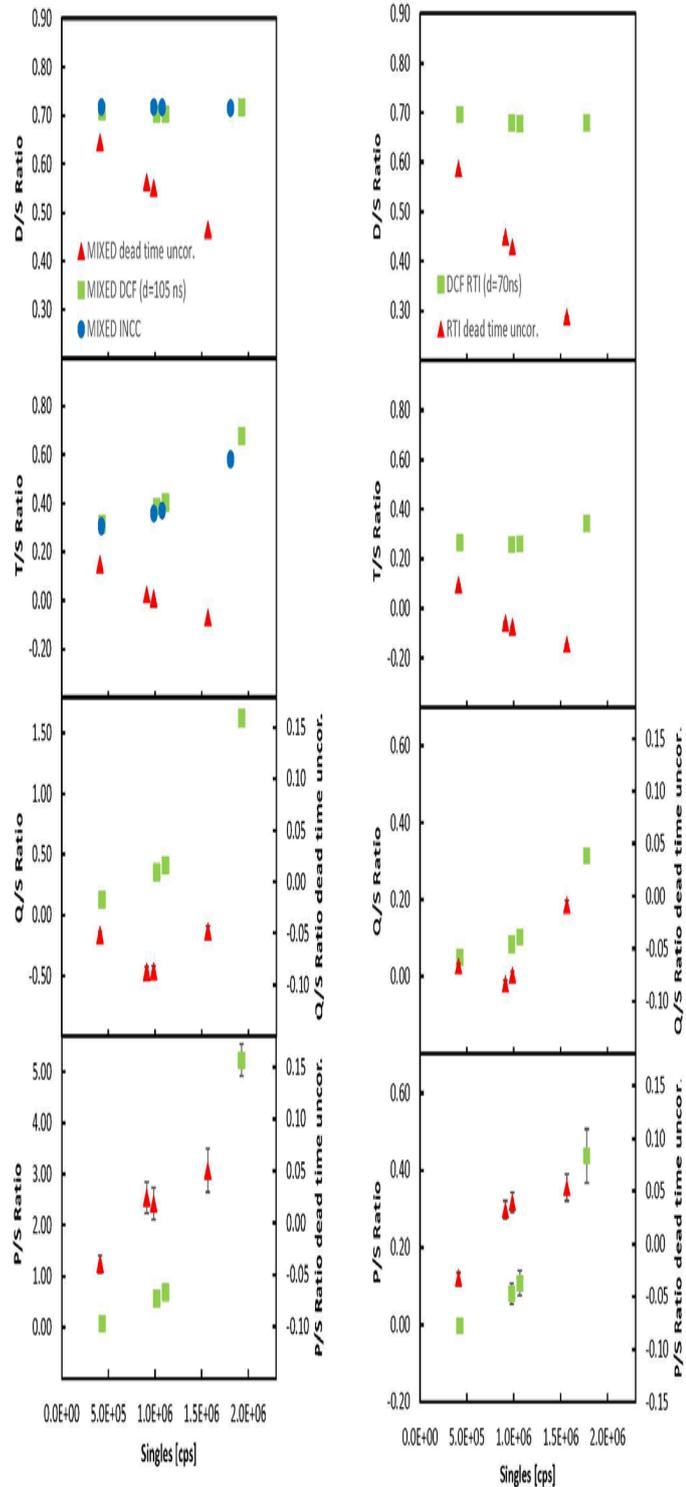


Figure3

